

Design and Development of Boring fixture for Connecting rodS.A.Raijada¹, A.L.Dudhatra²¹P.G. Student, Mechanical Engineering Dept, A.I.T.S, Rajkot, India²Asst. Professor, Mechanical Engineering Dept, A.I.T.S, Rajkot, India

Abstract-Connecting rod is key piece of engine. It ought to be precisely machined with the obliged resilience. Additionally the varieties of measurements in work-piece to work piece ought to be low so it will be simpler to amass in engine. At the same time, it has been watched that in the majority of the cases the process duration needed for machining (boring) the connecting rod was an excess of furthermore with the lower resilience precision in exhausting operation because of traditional installation. The diameters required of the smaller end and the Bigger end of the said connecting rod are 35.6 ± 0.010 mm and 55.6 ± 0.02 mm respectively. The aim of this project is to design and development of a new fixture for machining (Boring) operation using designing softwares i.e. Pro E. Because of varieties in diameters of the end side the rejection rate is high so with this new outline the point is to reduce the rejection rate up to 5% which is 13% presently furthermore to expand the production rate up to 10% to 15%.

Keyword-Connecting rod ;clapmings;lclator ; Iscar online calcualtion;Creo 3.0(PRO E)

I. INTRODUCTION

A fixture is a production tool that locates, holds, and supports the work securely so the required machining operations can be performed easily. Set blocks and feeler or thickness gauges are used with fixtures to guide the cutter to the work-piece. A fixture should be securely fixed to the table of the machine upon which the work is done. Though largely used on milling machines, fixtures are also designed to hold work for various operations on most of the well-known machine tools. Fixtures are production work-holding devices used to manufacture duplicate parts accurately. The correct relationship and alignment between the cutter, or other tool, and the work- piece must be maintained. To do this, a fixture is designed and built to hold, support, and locate every part to ensure that each is drilled or machined within the specified limits. The difference between the jig and fixture is in the way the tool is guided to the work-piece. Fixtures vary in design from relatively simple tools to expensive, complicated devices. Fixtures also help to simplify metalworking operations performed on special equipment.[1]

A. Classification of Fixture

Fixtures are typically grouped by the sort of machine on which they are utilized. Apparatuses can likewise be recognized by a sub characterization. Case in point, if a fixture is intended to be utilized on a milling machine, it is known as a milling Machine. On the off chance that the undertaking it is planned to perform will be straddle processing, it will be called a straddle-milling Fixture. The same rule applies to a machine installation that is intended to machine radii. It is known as a machine sweep Fixture.

The following is a partial list of production operations that use fixtures.

- Assembling
- Boring
- Broaching
- Drilling
- Forming
- Gauging
- Grinding

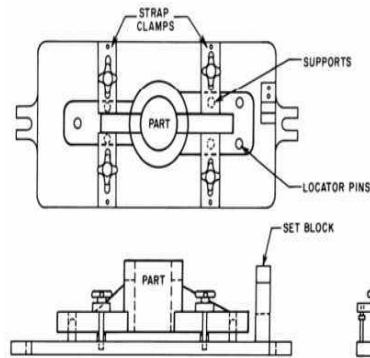


Figure 1. Plate Fixture [1]

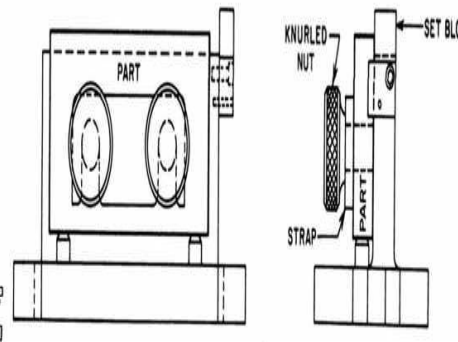


Figure 2. Angle plate Fixture [1]

Plate fixtures are the simplest form of fixture (Figure 1). The basic fixture is made from a flat plate that has a variety of clamps and locators to hold and locate the part. The **angle-plate fixture** is a variation of the plate fixture (Figure 1.2). With this tool, the part is normally machined at a right angle to its locator. While most angle-plate fixtures are made at 90 degrees, there are times when other angles are needed. [2]

B. Elements of Fixtures

* **Locators:** A locator is usually a fixed component of a fixture. It is used to establish and maintain the position of a part in the fixture by constraining the movement of the part. For work-pieces of greater variability in shapes and surface conditions, a locator can also be adjustable.

* **Clamps:** A clamp is a force-actuating mechanism of a fixture. The forces exerted by the clamps hold a part securely in the fixture against all other external forces.

* **Supports:** A support is a fixed or adjustable element of a fixture. When severe part displacement/deflection is expected under the action of imposed clamping and processing forces, supports are added and placed below the work-piece so as to prevent or constrain deformation. Supports in excess of what is required for the determination of the location of the part should be compatible with the locators and clamps.

* **Fixture Body:** Fixture body, or tool body, is the major structural element of a fixture. It maintains the spatial relationship between the fixturing elements mentioned above, viz., locators, clamps, supports, and the machine tool on which the part is to be processed. [2]

II. LITERATURE REVIEW

Previously all the work related to fixture design based on two factors first was to minimize some parameters which will ultimately increase the output i.e. The deflection, Vibrational effects, Rejection rate, Cycle time etc.

Maximization parameters i.e. Productivity, Immobilization Capability of fixture etc.

All the above parameters are to be optimized are based on the type of the operation for which the fixture is used.

After reading various papers related to the stated fixture design many methodologies are available. In which three methodologies are used in this research which are (1) Computer Aided Fixture Design (2) Case Based Reasoning (3) Feature Based Fixture.

III. PROBLEM DEFINITION

The major problem in existing fixture is the diameter dimensions which are not achieved in tolerances continuously. The diameters of the bigger end and the smaller end of the said connecting rod are $55.6 \pm 0.020 \text{ mm}$ and $35.6 \pm 0.010 \text{ mm}$ respectively according to customer's order. Which is quite difficult to achieve on a continuous basis. Due to which the rejection rate is high. Also the production rate with this existing fixture is low so with the new design the aim is to overcome the above stated problems. Figure below shows the existing fixture with its model.

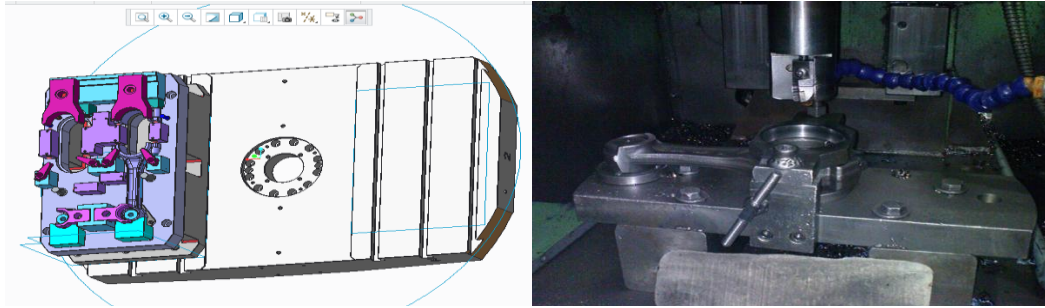


Figure 4.Existing old fixture with its CAD model prepared in creo 3.0

This is a existing mechanical fixture used in the company. Material use for connecting rod is:-S48c forged steel

IV. Design and Development of new fixture

First of all a base plate is designed for new fixture which is based on the dimensions of the said connecting rod. This base plate is designed using creo 3.0 Pro Engineering software. The figure below shows the CAD model of the Base plate and Connecting rod .

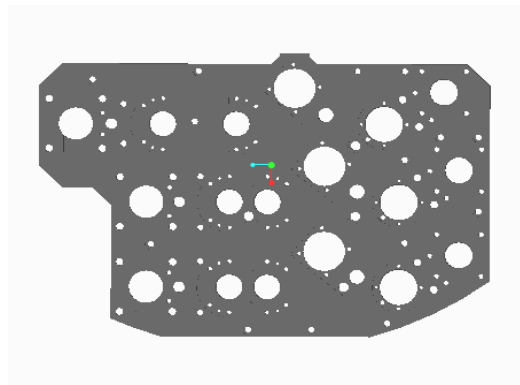


Figure 5.Base Plate

A.Thickness calculation of the base plate

The thickness of the Plate is determined by considering the plate as a simply supported beam as shown in fig below. The length and width of the plate is determined from the conrod dimensions and apex table of the SX 4 VMC on which the fixture is mounted.

B. calculation for thickness

$$\begin{aligned} \text{Total load} &= \text{wt. of component} + \text{wt. of other element on plate} & 134.5 \\ + & 63.78 \\ = & 198.28\text{N} \end{aligned}$$

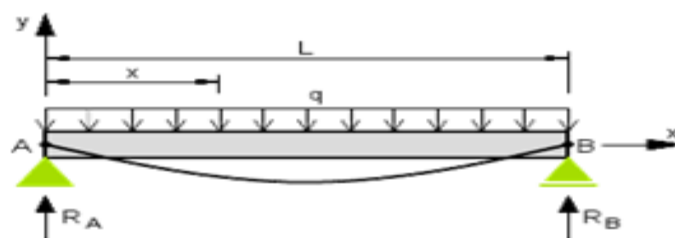


Figure 6.simply supported beam[3]

for MS plate...,

$$E = 21000 \text{ MPa} = 21 \times 10^9 \text{ N/m}^2$$

Maximum permissible deflection

$$\delta_{\max} = 0.01 \text{ mm} = 10^{-5} \text{ m}$$

$$\delta_{\max} = \frac{(5 \times w \times l^4)}{384 \times E \times I}$$

$$I = \frac{5 \times 200 \times 0.582^4}{384 \times 21 \times 10^4}$$

$$= 1.422 \times 10^{-6} \text{ m}$$

W= weight on plate (i.e. w=198.28 ≈ 200N)

l = Length of the plate (i.e. l= 582mm=0.582m)

I=Moment of inertia ,m⁴

$$I = \frac{b \times d^3}{12}$$

(Considering rectangular section)

b =Width of the plate =351m=0.351mm

d = Thickness of the plat

$$d^3 = \frac{12 \times I}{b}$$

$$= \frac{12 \times 1.422 \times 10^{-6}}{0.351}$$

$$= 4.8615 \times 10^{-5}$$

$$d = 0.036 \text{ m} = 36 \text{ mm ,thickness of the plate}$$

1. Clamping Device Calculation

Calculations forCutting Force

For cutting force calculation ,CMTI design data book is used which forms a standard base for the calculation .

Sr no.	Parameter	Meaning	Unit
1	<i>vc</i>	Cutting speed	m/min
2	<i>D</i>	Cutter diameter	mm
3	<i>n</i>	Spindle speed	rpm
4	<i>Vf</i>	Table feed or feed speed	mm/min
5	<i>fz</i>	Feed/tooth	mm
6	<i>Zc</i>	Number of effective teeth	no.
7	<i>ap</i>	Depth of cut	mm
8	<i>Q_{ro}</i>	Metal removal rate	mm ³ /min
9	<i>Ps</i>	power at spindle	kW

10	P_z	Tangential cutting force	N
11	K_c	Specific cutting force	N

Table 1.Parameter table [4]

The above parameters are used for the calculation of the cutting force and the clamping force.

FOR SMALLER END

1 Cutting speed (n):

$$V_c = \pi \times D_b \times n / 1000$$

$N = 1637$ rpm (Machine specification)

$D = 35$ mm

$$V_c = 3.14 \times 35 \times 1637 / 1000$$

$V_c = 180$ m/min

2 Feed per revolution (fn)

$$f_n = z_c \times f_z$$

$f_z = 0.08$ (as per standard tooling)

$$f_n = 1 \times 0.08$$

$f_n = 0.08$ mm/r

3 Power at the spindle (Ps)

$$P_s = ((a_p \times K_c \times f_n \times V_c) \div 60000) \left(1 - \frac{a_p}{d_c}\right)$$

$$= ((1.5 \times 2738 \times 0.08 \times 180) \div 60000) (1 - 1.5/35)$$

$$= 0.94 \text{ KW}$$

4 Metal Removal Rate

$$Q = (D_b \times f_n \times 180) / 4$$

$$Q = (35 \times 0.08 \times 180) / 4 = 19.62 \text{ mm}^3/\text{min}$$

5 Mean Torque

$$T_m = \frac{P_s \times 30000}{\pi \times n}$$

$$= (0.94 \times 30000) \div (\pi \times 1637) = 5.45 \text{ Nm}$$

Machining Force Calculation by ISCAR Tool Software For Smaller end Boring Operation (For finding of tangential force)

Boring

Insert Type: straight edge

Data for straight edge

Workpiece diameter (D): 35 mm

Feed per revolution (f): 0.08 mm

Depth of cut (ap): 1.5 mm

Spindle speed (n): 1637 rpm

Cutting velocity (Vc): 180 m/min

Workpiece material: S48C

Effective rake angle (gamma): 0 deg.

Lead angle (k): 55 deg.

Results

Kc: 2738 N/mm² 390 KPsi

Net power demand: 0.94 KW 1.28 HP

Material removal rate: 20.67 mm³/min 1.26 in³/min

Tangential force: 329 N 73.96 lb

Mean torque: 5.5 Nm 48.7 inch*lb

Calculate

Figure 7. Online Machining using ISCAR Software[5]

An online software is used, called ISCAR tool, for finding out the tangential force required for the connecting rod boring operation. In the above result, the values which are in the white box are calculated using standard design data book. While putting these values in the stated software, it gives the tangential force required as shown in the figure. Based on that force, clamping force is calculated. Same calculation is done for bigger end of the said connecting rod.

PARAMETER	VALUE	UNIT
Cutting Speed	180	m/min
Feed per revolution	0.08	mm/r
Power at the spindle	0.96	KW
Mean Torque	8.8	N.m
Metal Removal Rate	21.01	m ³ /min
Tangential force	329	N
Total Tangential Force	329	N

Table 2. Parameter table for bigger end dia.

Online Calculation for bigger end

As shown in above figure the same online calculation is made for the smaller end connecting rod. And in both the case the tangential force is same, which is 329 N given from the result.

2 Selection of Clamping Devices Boring operation

As per the above analytical and online calculation it is found that the tangential force for both ends are same which is 329 N. Now here the insert used for the operation is only 1. So tangential force per insert is $329 \times 1 = 329$ N. The clamping force must be more than the cutting force so we are taking the clamping force 5 times the tangential force. So the clamping force required for clamp the con rod is $329 \times 5 = 1645$ N. so there are 3 clamps used, so this 1645 is equally distributed to these 3 clamps.

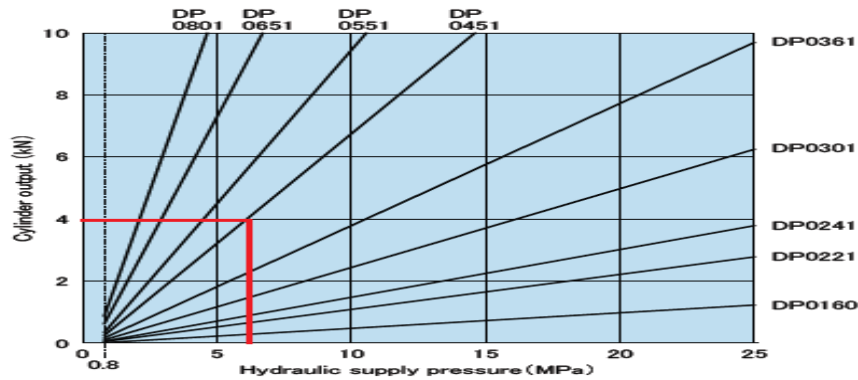


Figure 9. Hydraulic clamping device selection chart[6]

The required pressure is 7 MPa so based on requirement DP0451 clamping device selected from the above chart, which satisfies the requirement. Here the hydraulic clamping device is selected because it gives the best result which is required.

A. Unit Design of Fixture using Creo 3.0 with modifications

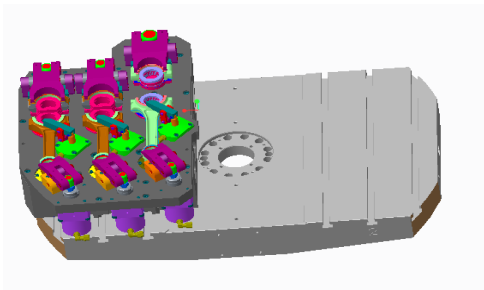


Figure 10. Unit Design with CAD model



Figure 11. Actual Fixture

V. VALIDATION OF THE DESIGN

Process Capability Analysis Based On Machining Trial

The case study shows the importance of statistical process control for monitoring and ensuring the product produced is able to satisfy customers' needs and requirements. A detailed study of manufacturing process was carried out for the elimination of the quality characteristic problem during milling operation. The focus of the study was to investigate the process capability of the ongoing process so as to decide upon the suitability of the machine to hold particular tolerance. In this study, in order to demonstrate the applicability of the proposed method and to make a clear decision about the capability of the machining process, the sample size was determined and a sufficient number of sample parts were inspected. A single sampling plan was implemented by using the lot-acceptance sampling plan. Samples were chosen randomly during the machining process.

A table below gives the values for the smaller end diameters which are measured from older fixture. In first step the process capability is calculated for the smaller end with older fixture.

Readings taken from the old fixture (smaller end)

		Sample Size			
		1	2	3	4
	Drg. Limits	35.6±0.010	35.6 ±0.010	35.6±0.010	35.6±0.010
	LSL	35.59	35.59	35.59	35.59
	USL	35.61	35.61	35.61	35.61

1	AK1	35.012	35.013	35.014	35.014
2	AK2	35.010	35.012	35.015	35.241
3	AK3	35.012	35.011	35.012	35.014
4	AK4	35.019	35.015	35.014	35.015
5	AK5	35.001	34.999	35.031	35.017
6	AK6	35.25	34.985	35.015	34.826
7	AK7	35.014	35.010	34.987	35.012
8	AK8	34.991	35.009	35.0.17	35.019
9	AK9	35.010	35.248	35.016	35.014
10	AK10	35.011	35.005	35.124	34.989
11	AK11	34.992	35.018	35.015	35.017
12	AK12	35.017	35.125	35.014	35.019
13	AK13	35.017	35.019	35.014	35.019
14	AK14	35.018	33.018	35.014	35.017
15	AK15	35.017	34.613	35.012	35.014
16	AK16	35.018	34.987	35.608	35.124
17	AK17	34.523	35.014	35.014	34.985
18	AK18	35.011	35.016	34.988	35.017
19	AK19	35.125	34.785	35.611	35.016
20	AK20	35.011	34.988	35.012	33.012
21	AK21	35.006	34.985	35.020	35.145
22	AK22	35.325	35.006	34.783	35.015
23	AK23	35.010	35.015	35.015	35.014
24	AK24	35.005	35.014	35.014	34.988
25	AK25	35.018	35.015	35.014	35.014
Mean of the process					
STDEV(σ)		0.130221	0.4099121	0.17832424	0.40828196
3*STDEV(σ)		0.390664	1.2297363	0.53497273	1.22484588
6*STDEV(σ)		0.781329	2.4594725	1.06994547	2.44969177
Cpu		0.00588	0.7548	0.0486	0.0628
Cpl		0.09650	0.00951	0.1445	0.0635
Cpk		0.00588	0.00951	0.0486	0.0628
Cp		0.051	0.016	0.037`	0.016
Acceptance Criteria		CpCpk 1.33	CpCpk 1.33	CpCpk 1.33	CpCpk 1.33

Readings taken from the modified fixture (Smaller end)

		Sample Size			
		1	2	3	4
	Drg. Limits	35 ±0.020	35 ±0.020	35 ±0.020	35 ±0.020
	LSL	35.02	35.02	35.02	35.02
	USL	34.98	34.98	34.98	34.98
1	AK1	35.607	35.599	35.604	35.606
2	AK2	35.607	35.599	35.604	35.604
3	AK3	35.597	35.597	35.601	35.607
4	AK4	35.601	35.604	35.6	35.603
5	AK5	35.598	35.598	35.603	35.603
6	AK6	35.597	35.6	35.603	35.607
7	AK7	35.6	35.604	35.6	35.607
8	AK8	35.598	35.6	35.6	35.603
9	AK9	35.605	35.605	35.597	35.604
10	AK10	35.598	35.603	35.606	35.604
11	AK11	35.597	35.597	35.6	35.603
12	AK12	35.6	35.604	35.6	35.603
13	AK13	35.605	35.6	35.603	35.603
14	AK14	35.603	35.605	35.603	35.603
15	AK15	35.597	35.603	35.6	35.603
16	AK16	35.601	35.597	35.6	35.603
17	AK17	35.6	35.604	35.603	35.603
18	AK18	35.604	35.6	35.605	35.605
19	AK19	35.598	35.605	35.604	35.604
20	AK20	35.6	35.598	35.604	35.604
21	AK21	35.598	35.597	35.602	35.602
22	AK22	35.6	35.598	35.602	35.603
23	AK23	35.601	35.598	35.6	35.6
24	AK24	35.605	35.598	35.6	35.6
25	AK25	35.598	35.6	35.599	35.602
Mean of the process		35.60044	35.60028	35.60172	35.60356
STDEV(σ)		0.003110	0.002879	0.002189	0.001804
3*STDEV(σ)		0.009330	0.008639	0.006568	0.0054138
6*STDEV(σ)		0.018661	0.017278	0.013136	0.0108277
Cpu		1.024	1.1250	1.26063	1.189
Cpl		1.1188	1.189	1.78438	2.5046
Cpk		1.024	1.1250	1.2606	1.189

Cp	1.0717	1.15	1.5225	1.84
Acceptance Criteria	CpCpk 1.00	CpCpk 1.00	CpCpk 1.00	CpCpk 1.00

From the above table it can be seen that the Cp and Cpk values for the old fixture does not satisfies the criteria where as in new fixture Cp and Cpk values are within the given criteria. Same procedure is applied to bigger end dia of the connecting rod .

VII. CONCLUSION

In every cycle , work pieces are clamped with same clamping force which is 1645 N. Compared to existing old fixture this new proposed fixture is stable and capable. By this new fixture design work pieces are clamped in same direction every time so a correct location is achieved and eliminating the variability in work piece deflection from clamping force. The results from the machining trial and process capability is stated below.

- Achieved connecting rod dimensions in given tolerance continuously which is 35.6 ± 0.010 mm and 55.6 ± 0.020 mm for smaller end and for bigger end respectively .
- Achieved process capability (Cp and Cpk) more than 1.00

REFERENCES

- [1] Edward G. Hoffman, Jig and Fixture design; 3rd Edition; Delmar Publishers Inc., Clifton Park, NY pp no. 8 to 20
- [2] P. C. Sharma, A Textbook of Production Engineering, S. Chand & Company Ltd., New Delhi 2006, pp no. 2 to 3,
- [3] Bela I. Sandor, Ryan Roloff, Stephen M. Birn, Mechanics of solid pp no 223
- [4] Design data book, CMTI
- [5] <http://mpwr.iscar.com/machiningpwr/machiningpower.wgx>
- [6] http://www.kosmek.co.jp/data/eng/pdf/new/DP001_04_02.pdf
- [7] Parvesh Kumar Rajvanshi And Dr. R.M. Belokar, "Improving the process capability of a boring operation by the application of statistical techniques", International Journal of Scientific & Engineering, 2012
- [8] www.jyoti.co.in/company_profile.aspx